

Università degli Studi di Padova – Dipartimento di Ingegneria Industriale

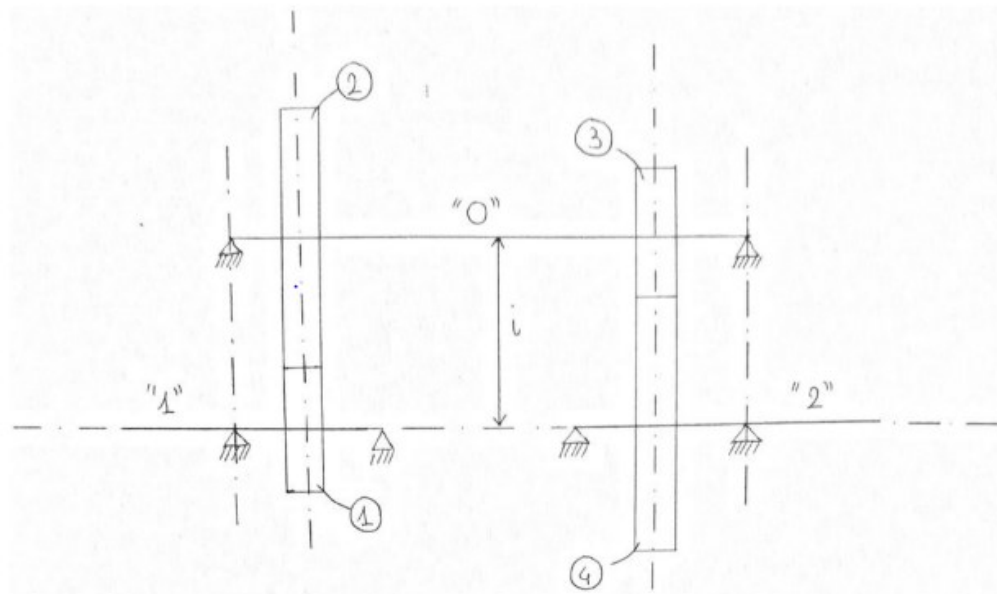
Corso di Laurea in Ingegneria Meccanica

Relazione per la prova finale
Progettazione strutturale di un riduttore ad
ingranaggi con assi paralleli e simulazione
tramite analisi agli elementi finiti

Tutor universitario: Prof. Meneghetti G.

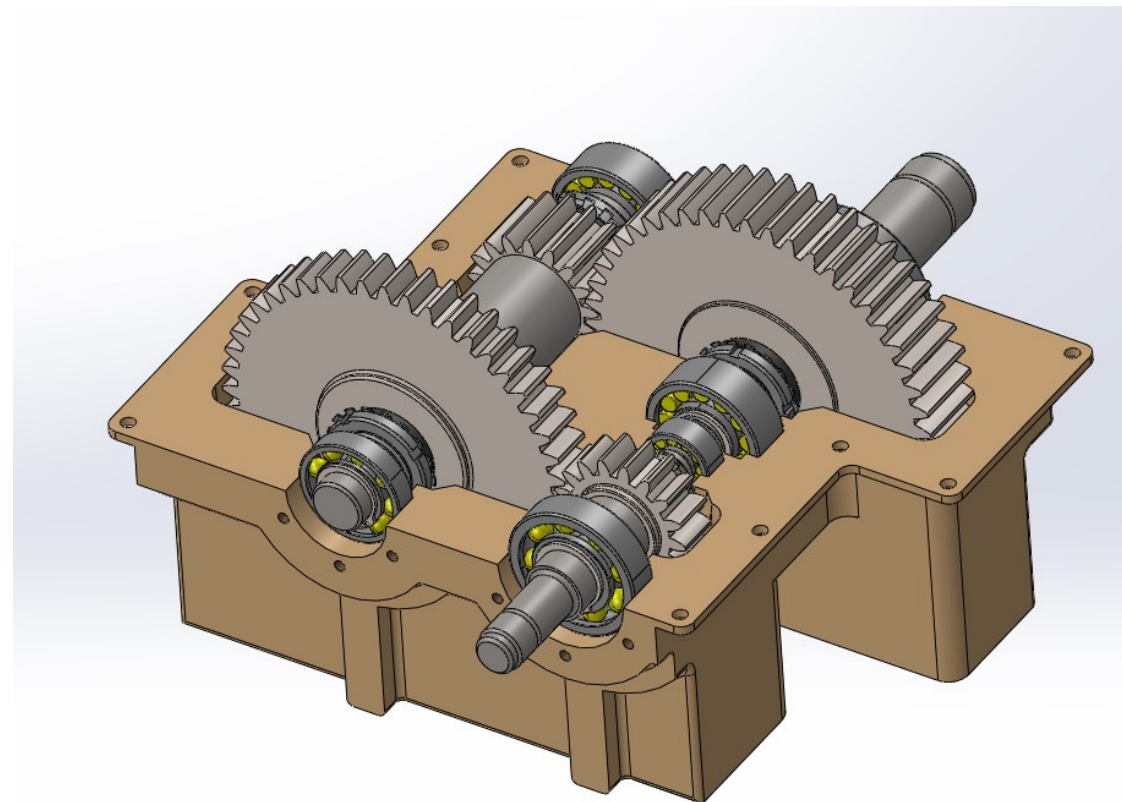
Laureando: *Caprari Leonardo 1216805*

Padova, 2021/2022



Viene interposto tra un albero motore ed un albero condotto al fine di ridurre il numero di giri ed aumentare il Momento torcente del secondo rispetto al primo.

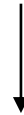
RIDUTTORE: dispositivo meccanico di trasmissione di potenza con un rapporto di riduzione $\tau > 1$.



OBIETTIVO: il riduttore verrà utilizzato per collegare coassialmente un motore elettrico asincrono trifase al tamburo di un nastro trasportatore che richiede da progetto una certa coppia nominale M_{R2} ad una certa velocità di rotazione nominale n_2

DATI	VALORI
M_{R2}	1300 Nm
n_2	176 giri/min
τ_{tot}	8

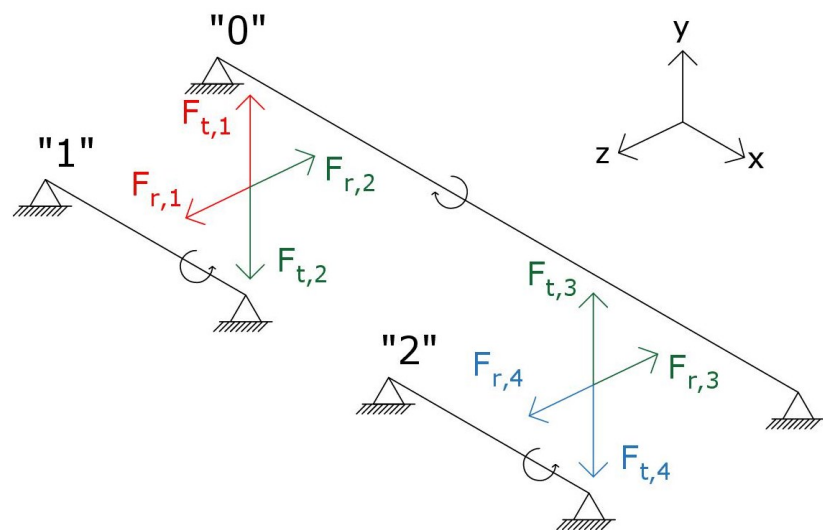
$$\longrightarrow \tau = \tau_{12} = \tau_{34} = \sqrt{\tau_{tot}} = \sqrt{8} \cong 2,83$$



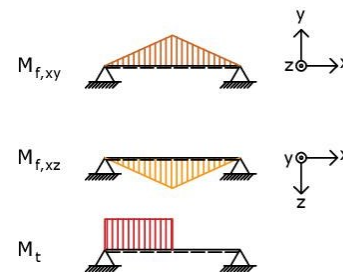
$$M_2 = M_{R2} \cdot f_s = 1300 \cdot 1,5 = 1950 \text{ Nm}$$

Albero	n [giri/min]	ω [rad/s]	P [kW]	M [Nm]
1	1409,57	147,61	38,99	264,19
0	498,08	52,16	37,44	717,75
2	176	18,43	35,94	1950,00

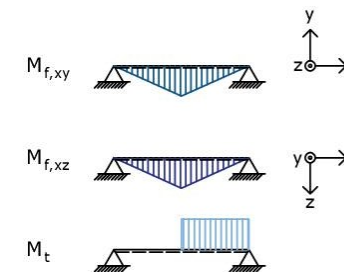
Ruota	Z	m [mm]	Dp [mm]	λ	b [mm]	i [mm]
1	17	5,5	93,5	6	33	178,75
2	48	5,5	264	6	33	
3	17	5,5	93,5	10	55	178,75
4	48	5,5	264	10	55	



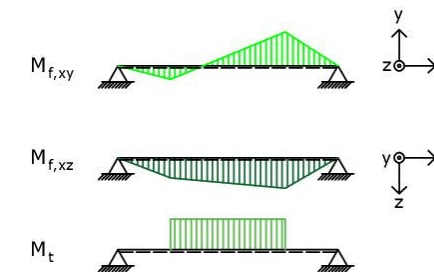
Albero 1



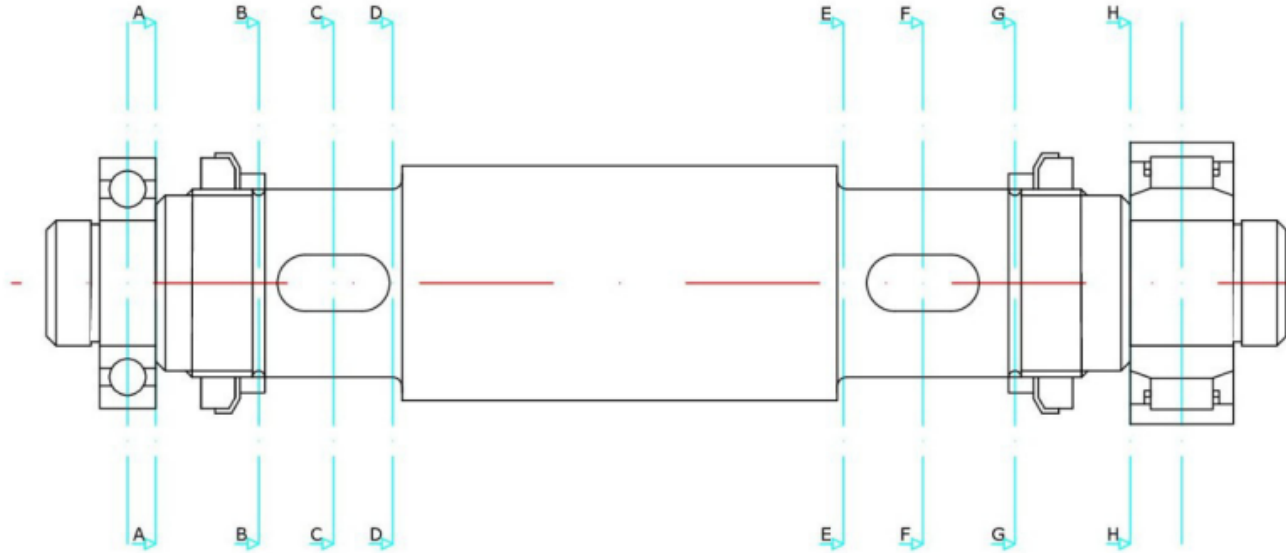
Albero 2



Albero 0



albero	F_r [N]	F_t [N]	M_f [Nmm]	M_t [Nmm]	σ_{id} [MPa]	y_s richiesto	d [mm]	y_s calcolato	L/d
1	2056	5651	198462	264190	78,43	7	34	7,161	3,88
0	5588	15352	948189	948189	53,43	10	60	10,487	5,63
2	5376	14772	652422	1950000	111,09	5	55	5,041	3,02



Sezione	d	M_{fxy}	M_{fyz}	M_f	W_f	W_t	σ_f	τ_{Mt}	σ_{id}	ν_s
[]	[mm]	[Nmm]	[Nmm]	[Nmm]	[mm ³]	[mm ³]	[MPa]	[MPa]	[MPa]	[MPa]
A-A	40	5454	26631	27184	6283	/	4,3	0	4,3	129
B-B	56	25452	124278	126858	17241	/	7,4	0	7,4	76,1
C-C	60	39996	195294	199348	21206	42411	9,4	16,9	30,8	18,2
D-D	60	66308	216854	226765	21206	42411	10,7	16,9	31,2	17,9
E-E	60	737956	353074	818071	21206	42411	38,6	16,9	48,4	11,6
F-F	60	873243	382464	953327	21206	42411	45,0	16,9	53,7	10,4
G-G	56	562874	246528	614494	17241	/	35,6	0	35,6	15,7
H-H	40	173597	76032	189517	6283	/	30,1	0	30,2	18,6

Sezione	σ_a	τ_{Mt}	K_d	K_l	K_f	$\sigma_{a\infty,-1}^*$	ν_f
[]	[MPa]	[MPa]	[]	[]	[]	[MPa]	[]
A-A	4,3	0	1,2	1,07	2,7	112,5	25,2
B-B	7,3	0	1,25	1,2	2,49	104,4	14,3
C-C	9,4	16,9	1,26	1,2	2,1	122,8	13,1
D-D	10,7	16,9	1,26	1,07	1,96	147,6	13,4
E-E	38,5	16,9	1,26	1,07	1,96	147,6	3,7
F-F	44,7	16,9	1,26	1,2	2,1	122,8	2,7
G-G	35,3	0	1,25	1,2	2,49	104,4	2,9
H-H	30,1	0	1,2	1,07	2,7	112,5	3,7

$$R_{sx,xy} = R_{dx,xy} = \frac{F_{t,1}}{2} = \frac{5651}{2} = 2825 \text{ N} \quad R_{dx,xz} = R_{dx,xz} = \frac{F_{r,1}}{2} = \frac{2056}{2} = 1028 \text{ N}$$

$$R_{sx} = \sqrt{R_{xs,xy}^2 + R_{xs,xz}^2} = \sqrt{2825^2 + 1028^2} = 3006 \text{ N}$$

$$R_{dx} = \sqrt{R_{dx,xy}^2 + R_{dx,xz}^2} = \sqrt{2825^2 + 1028^2} = 3006 \text{ N}$$

$$L_{10} = \frac{60 n_1 L_{10h}}{10^6} = \frac{60 \cdot 1409,57 \cdot 40000}{10^6} = 3383 \text{ milioni di giri}$$

$$\sigma_{adm} = \frac{\sigma_s}{v_s} = \frac{420}{1,5} = 280 \text{ MPa} \quad \tau_{adm} = \frac{\sigma_{adm}}{\sqrt{3}} = \frac{280}{\sqrt{3}} = 161 \text{ MPa}$$

$$l = 2 \frac{M_{t1}}{d_1 t_1 p_c} = 2 \frac{264190}{34 \cdot 5 \cdot 90} = 34,53 \text{ mm} \rightarrow \text{scelgo } l = 36 \text{ mm}$$

$$\tau = 2 \frac{M_{t1}}{d_1 b l} = 2 \frac{264190}{34 \cdot 10 \cdot 36} = 43,168 \text{ MPa} < \tau_{adm} = 161 \text{ MPa}$$

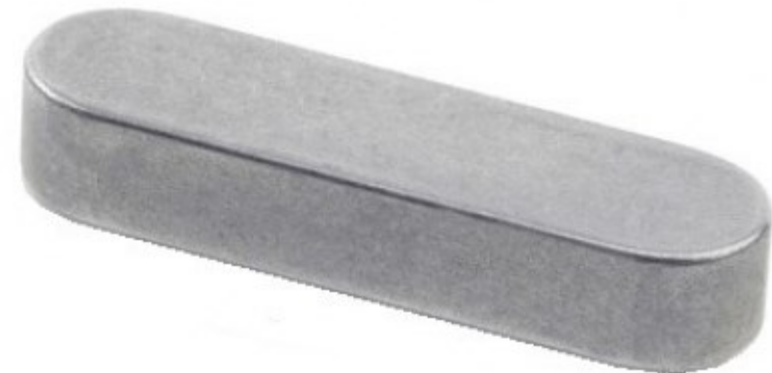
Cuscinetto sinistro SKF 6309

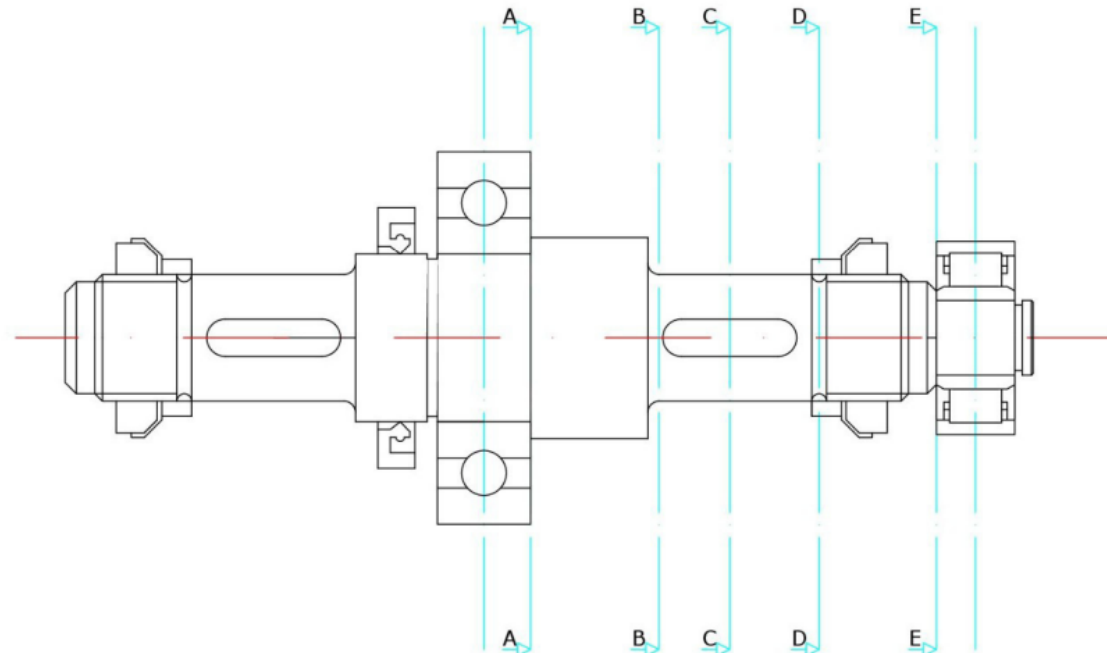
$$C = L_{10}^{\frac{1}{3}} \cdot R_{dx} = 3383^{\frac{1}{3}} \cdot 3006 = 45124 \text{ N}$$

Cuscinetto destro SKF NU 2304 ECP

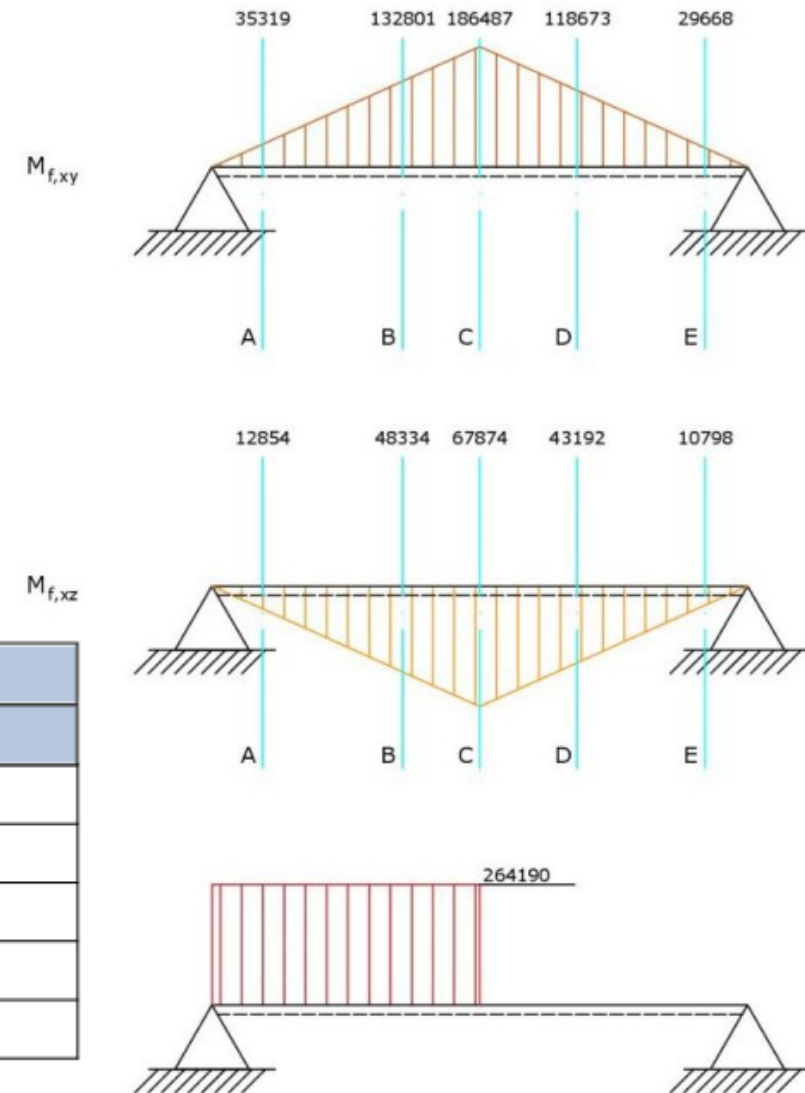
$$C = L_{10}^{\frac{3}{10}} \cdot R_{dx} = 3383^{\frac{3}{10}} \cdot 3006 = 34417 \text{ N}$$

B 10×8×36 UNI 6604





Sez.	d	σ_a	τ	K_d	K_l	K_r	σ'_{a,σ_v-1}	v_r
	[mm]	[MPa]	[MPa]				[MPa]	
AA	45,00	4,20	14,77	1,22	1,07	2,49	119,98	28,57
BB	34,00	36,63	34,23	1,18	1,07	2,1	147,52	4,03
CC	34,00	51,43	34,23	1,18	1,20	2,1	131,54	2,56
DD	32,00	39,26	0,00	1,16	1,20	2,18	128,51	3,27
EE	20,00	40,20	0,00	1,10	1,07	2,21	149,93	3,73



$$R_{sx,xy} = R_{dx,xy} = \frac{F_{t,4}}{2} = \frac{14772}{2} = 7386 \text{ N} \quad R_{dx,xz} = R_{dx,xz} = \frac{F_{r,4}}{2} = \frac{5376}{2} = 2688 \text{ N}$$

$$R_{sx} = \sqrt{R_{xs,xy}^2 + R_{xs,xz}^2} = \sqrt{7386^2 + 2688^2} = 7860 \text{ N}$$

$$R_{dx} = \sqrt{R_{dx,xy}^2 + R_{dx,xz}^2} = \sqrt{7386^2 + 2688^2} = 7860 \text{ N}$$

Cuscinetto destro SKF 6214

$$C = L_{10}^P \cdot R_{dx} = 422,4^{\frac{1}{3}} \cdot 7860 = 58974 \text{ N}$$

Cuscinetto sinistro Nu 2308 ECP

$$C = L_{10}^P \cdot R_{dx} = 422,4^{\frac{3}{10}} \cdot 7860 = 48210 \text{ N}$$

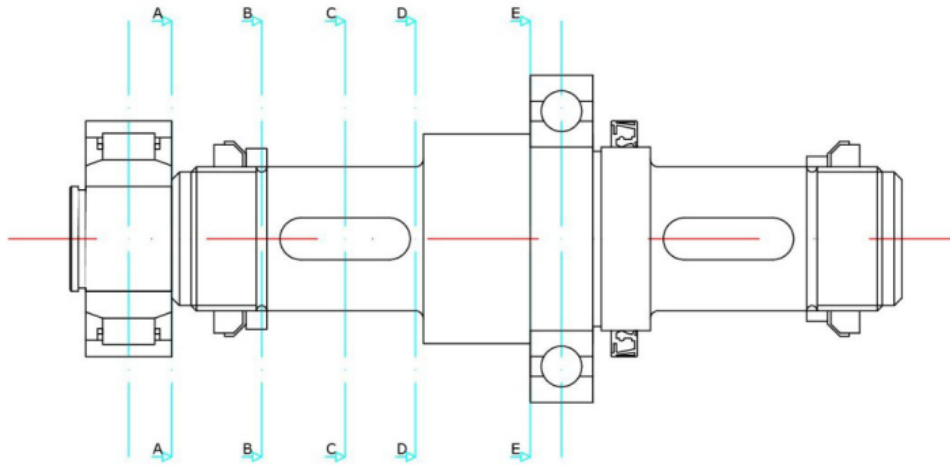
$$\sigma_{adm} = \frac{\sigma_s}{v_s} = \frac{420}{1,5} = 280 \text{ MPa} \quad \tau_{adm} = \frac{\sigma_{adm}}{\sqrt{3}} = \frac{280}{\sqrt{3}} = 161 \text{ MPa}$$

$$l = 2 \frac{M_{t2}}{2 \cdot d_1 t_1 p_c} = 2 \frac{1950000}{2 \cdot 55 \cdot 6 \cdot 105} = 48,23 \text{ mm} \rightarrow \text{scelgo } l = 50 \text{ mm}$$

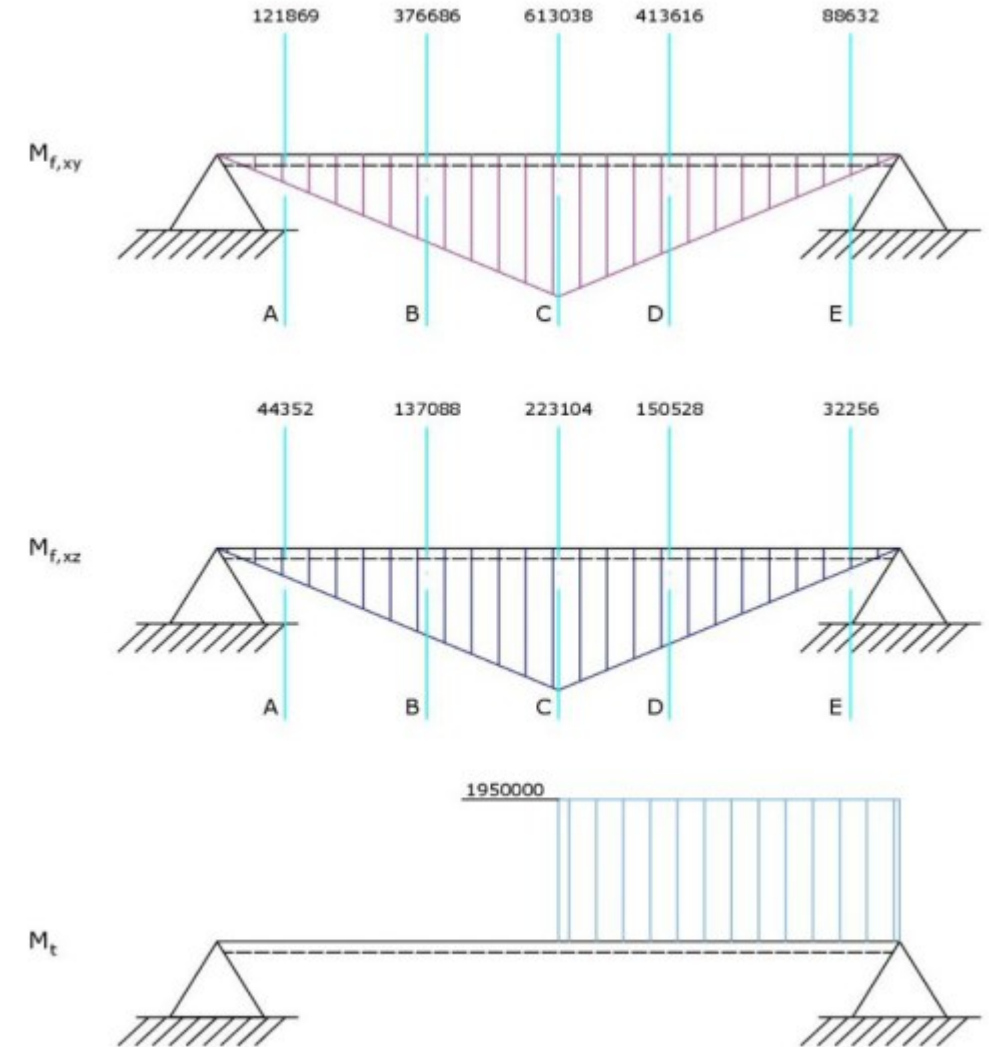
$$\tau = 2 \frac{M_{t1}}{d_1 b l} = 2 \frac{1950000}{2 \cdot 55 \cdot 16 \cdot 50} = 44,318 \text{ MPa} < \tau_{adm} = 161 \text{ MPa}$$

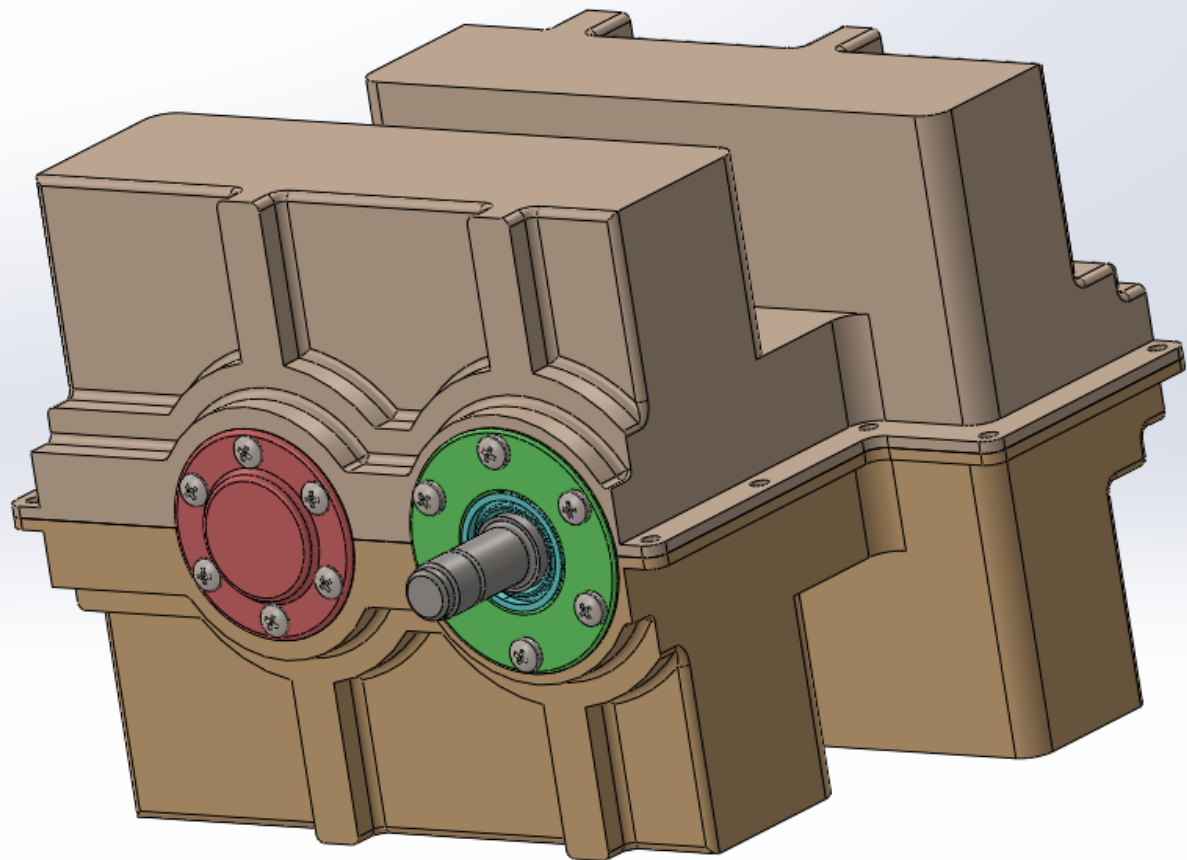
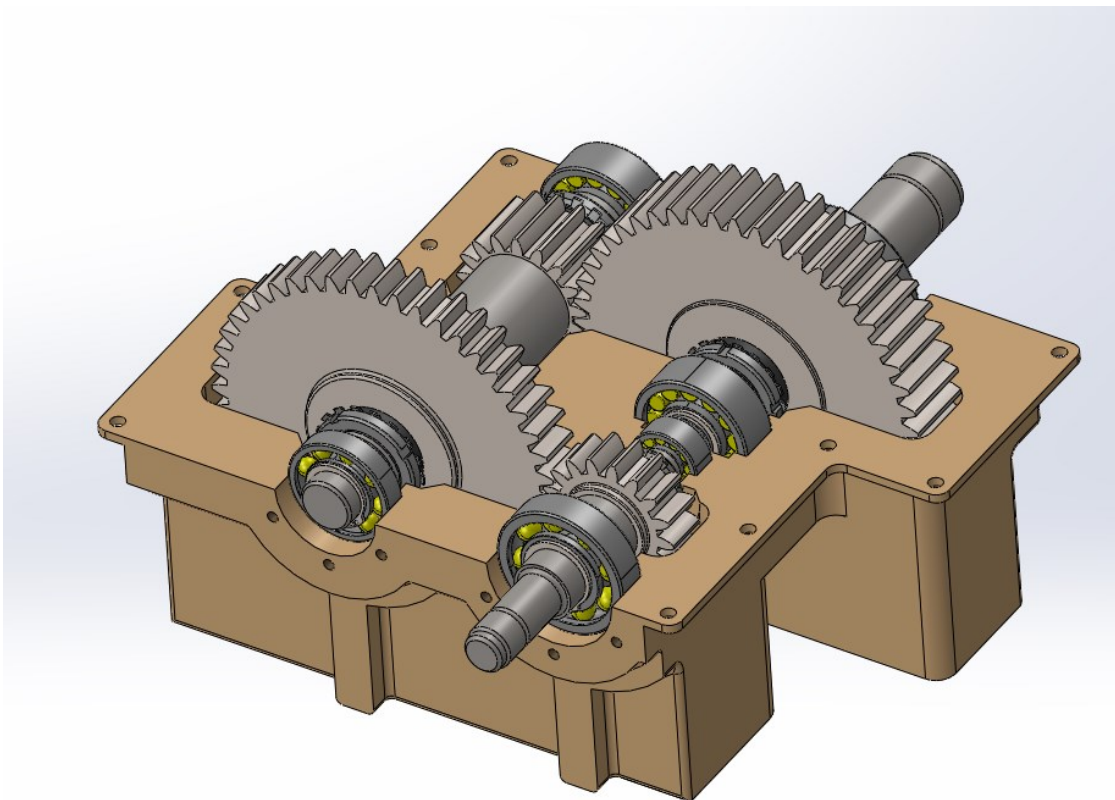
2 linguette

B 16×10×50 UNI 6604

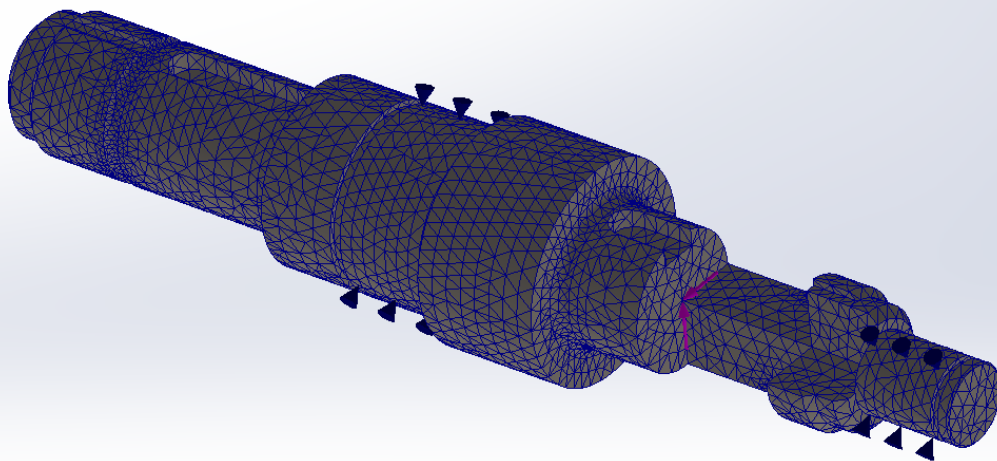


Sez.	d	σ_a	τ	K_d	K_l	K_f	$\sigma'_{a,\sigma-1}$	v_f
[]	[mm]	[MPa]	[MPa]	[]	[]	[]	[MPa]	[]
AA	40,00	20,64	0,00	1,20	1,07	2,47	122,97	5,96
BB	51,00	30,78	0,00	1,24	1,20	2,16	121,83	3,96
CC	55,00	39,94	59,69	1,25	1,20	2,1	124,21	3,11
DD	55,00	26,95	59,69	1,25	1,07	2,08	140,64	5,22
EE	70,00	2,80	28,95	1,28	1,07	2,28	124,82	44,56



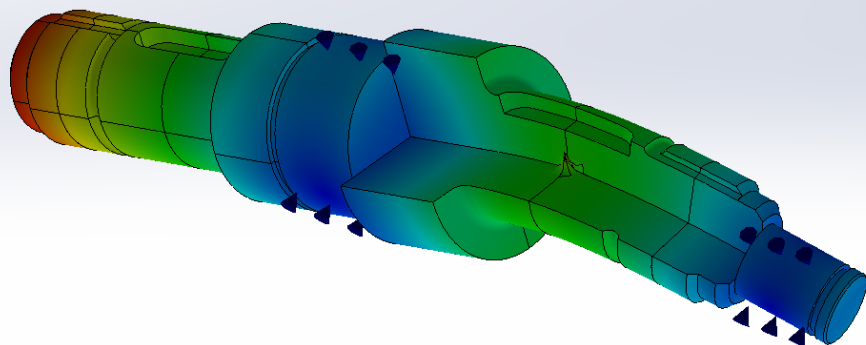
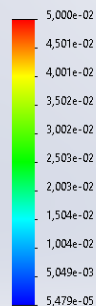


ALBERO DI INGRESSO

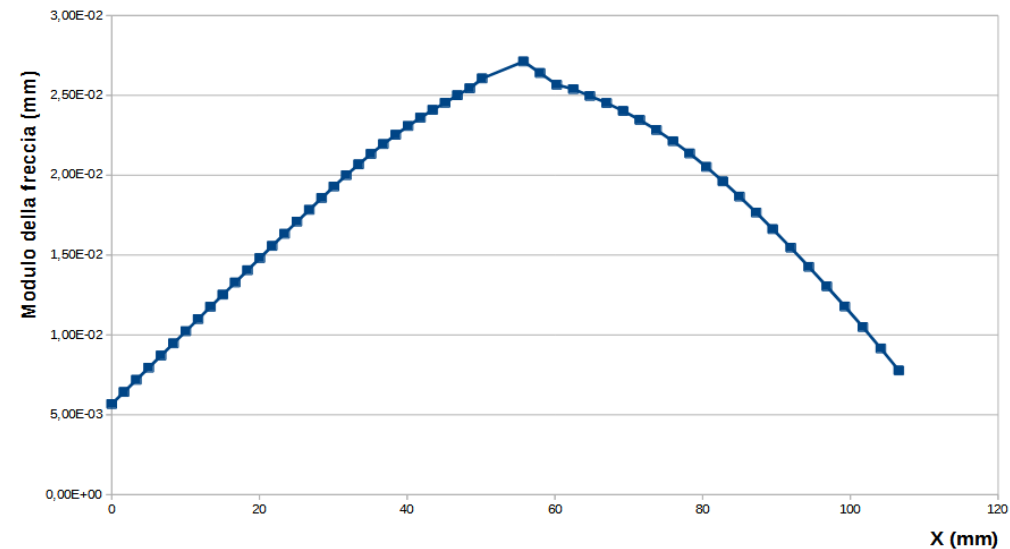


Model name: albero_1
Study name: studio statico albero 1(-Default-)
Plot type: Static displacement Displacement1
Deformation scale: 548,416

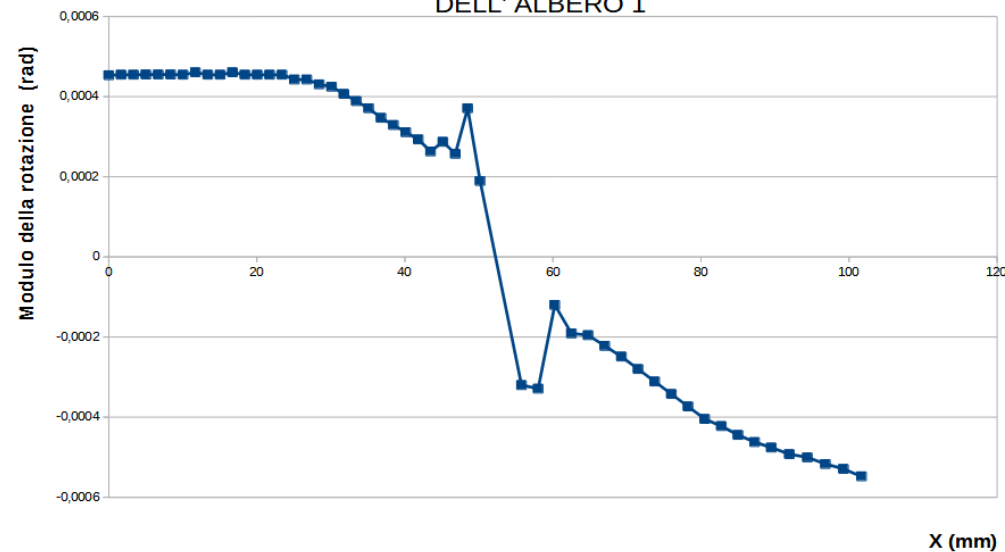
URES (mm)



ANDRAMENTO DELLA SPOSTATA LUNGO L' ALBERO 1

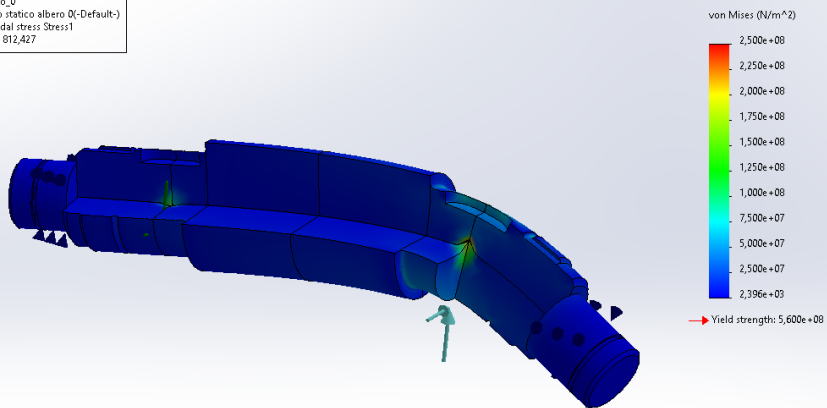


ANDAMENTO DELL'ANGOLO DI INCLINAZIONE DELL'ASSE DELL' ALBERO 1

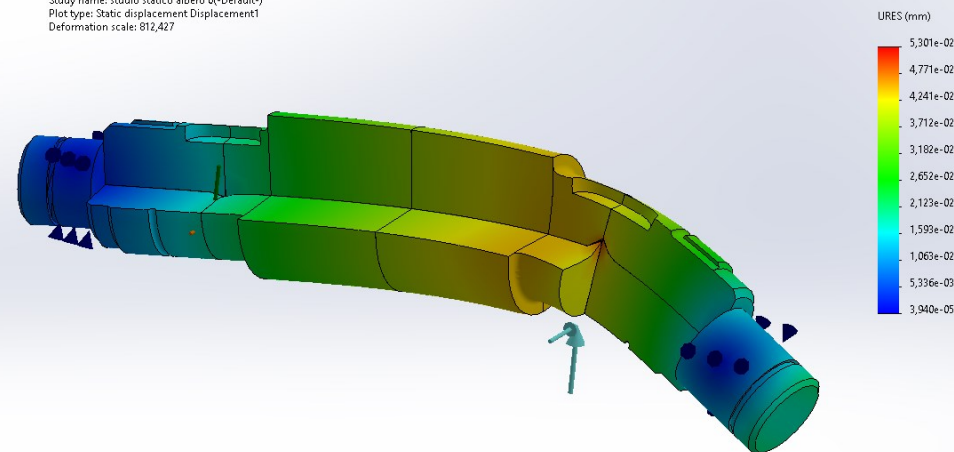


ALBERO INTERMEDIO

Model name: albero_0
Study name: studio statico albero 0(-Default-)
Plot type: Static nodal stress Stress1
Deformation scale: 812,427

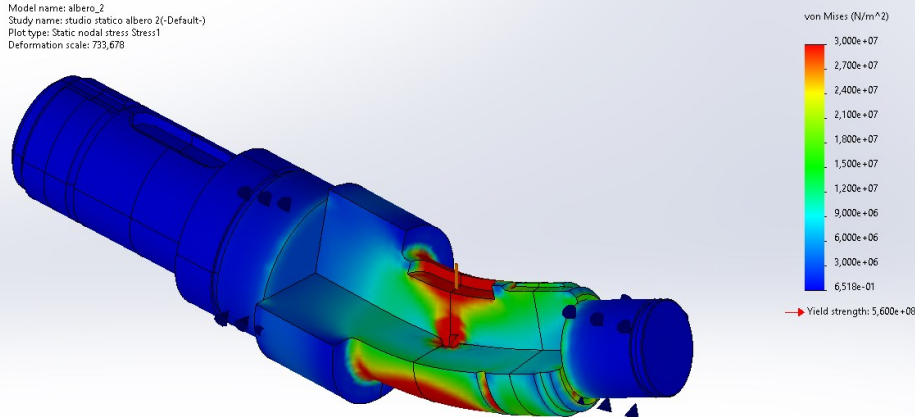


Model name: albero_0
Study name: studio statico albero 0(-Default-)
Plot type: Static displacement Displacement1
Deformation scale: 812,427

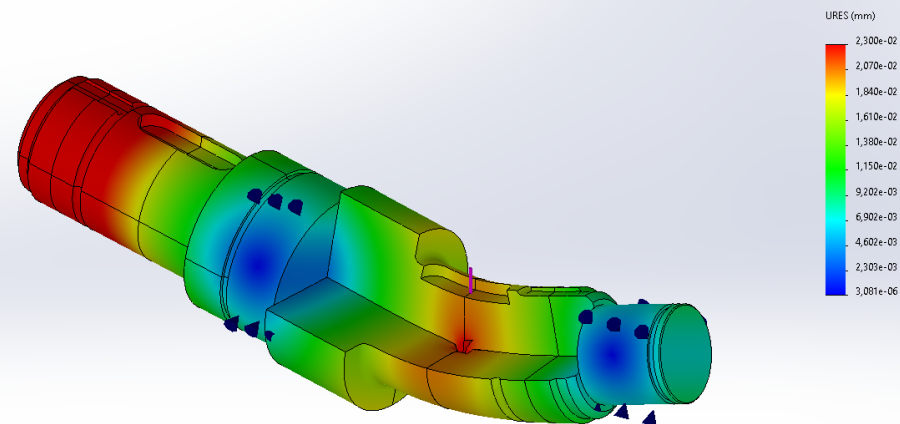


ALBERO DI USCITA

Model name: albero_2
Study name: studio statico albero 2(-Default-)
Plot type: Static nodal stress Stress1
Deformation scale: 733,678



Model name: albero_2
Study name: studio statico albero 2(-Default-)
Plot type: Static displacement Displacement1
Deformation scale: 733,678



- Verifica statica ✓
- Verifica a fatica ✓
- Verifica a deformazione

FORMULE ✓

FEM ✓

IMPRECISIONI

- Occorre affinare il modello mesh
- Studio più accurato della cassa del riduttore
- Mancanza di informazioni sul budget di progetto