

“SVILUPPO DI UN’ALA POSTERIORE, CON SISTEMA DRS, PER UNA VETTURA DI FORMULA SAE”

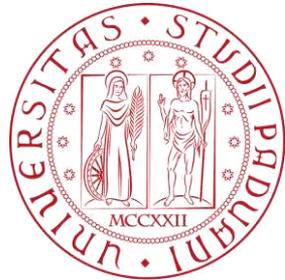
DIPARTIMENTO DI INGEGNERIA INDUSTRIALE

CORSO DI LAUREA TRIENNALE IN INGEGNERIA AEROSPAZIALE

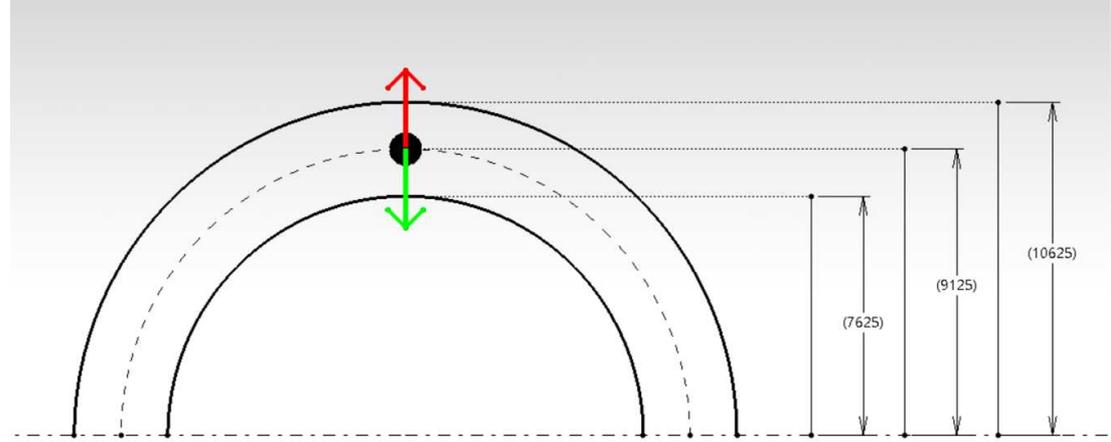
Relatore: Prof. Francesco Picano

Laureando: Bisson Christian

Matricola: 1226123

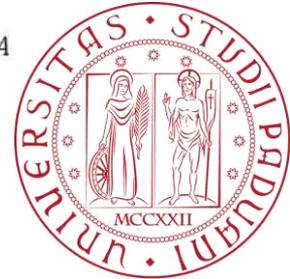


PERCHE' USARE L'AERODINAMICA

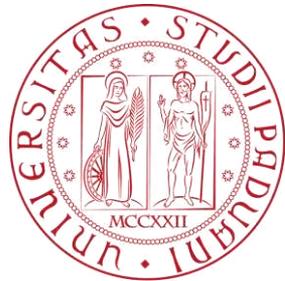
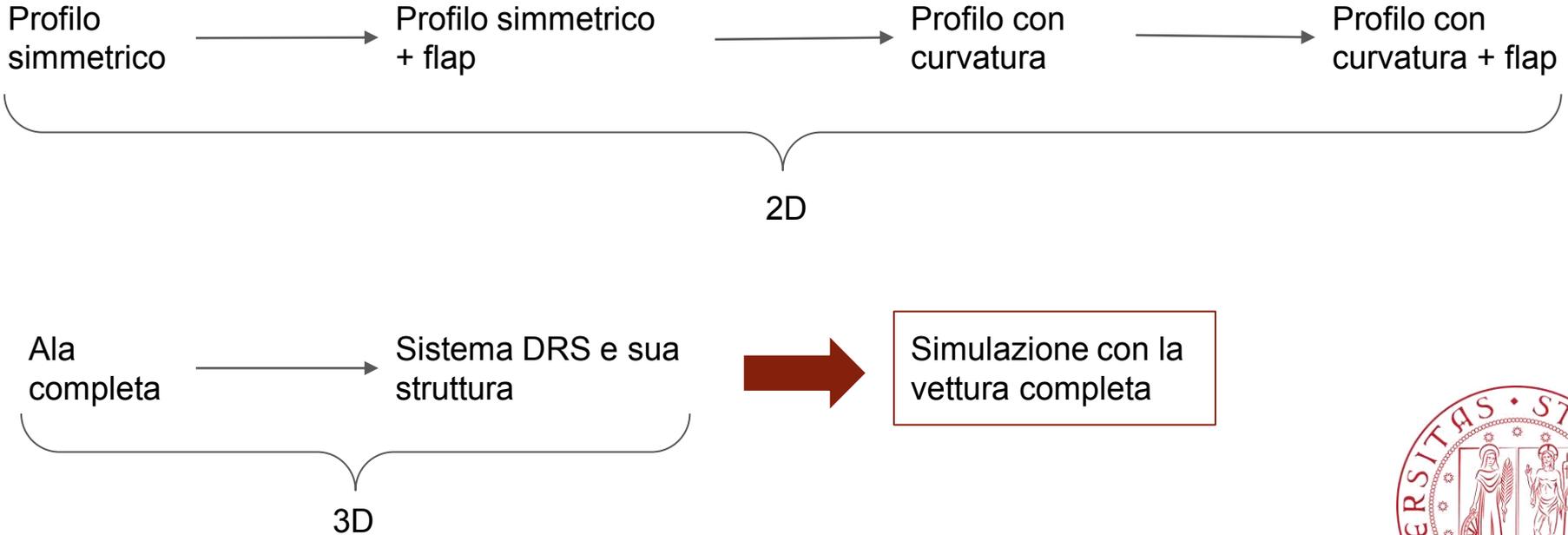


MASSA	IRRILEVANTE	180 kg
COEFFICIENTE DI ATTRITO	0.97	0.97
CLA AEROPACK	NESSUNO	3 m ²
TEMPO DI PERCORRENZA	<u>12.26 s</u>	<u>11.67 s</u>

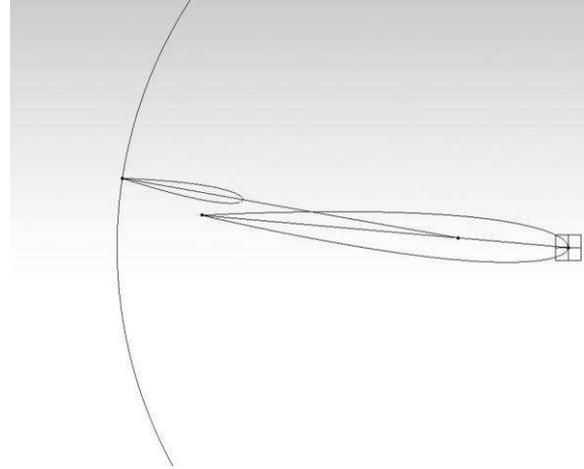
$$\left\{ \begin{aligned}
 F_{CF} &= F_{CP} \Leftrightarrow m \frac{v^2}{r} = F_{\perp} \mu_a \\
 F_{\perp} &= mg + F_{aero} \\
 F_{aero} &= \frac{1}{2} \rho V_{\infty}^2 C_{LA}
 \end{aligned} \right.$$



LE FASI DELLO STUDIO

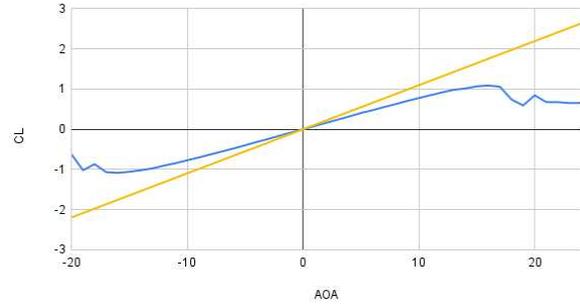


PROFILO SIMMETRICO NACA 0012

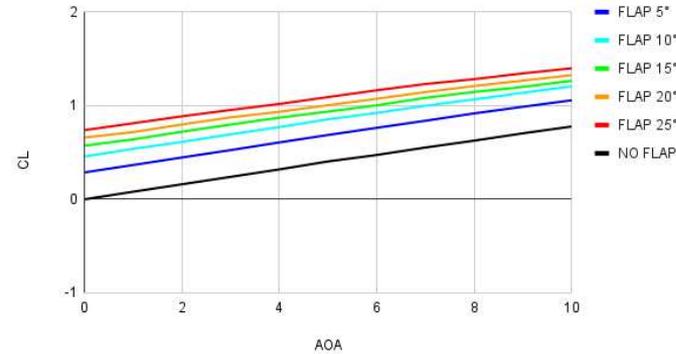


$$C_L = 2\pi(\alpha - \alpha_0)$$

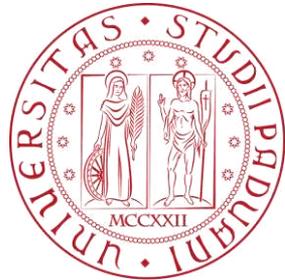
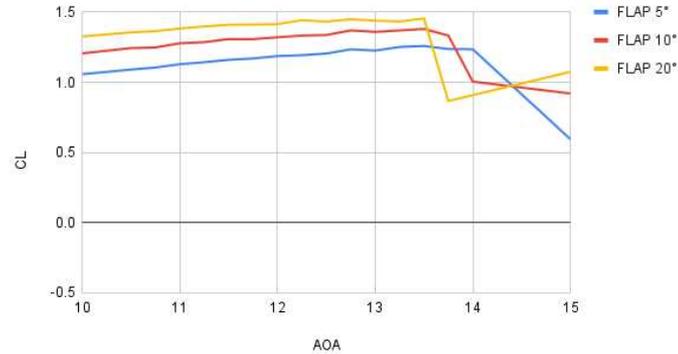
NACA 0012 C650



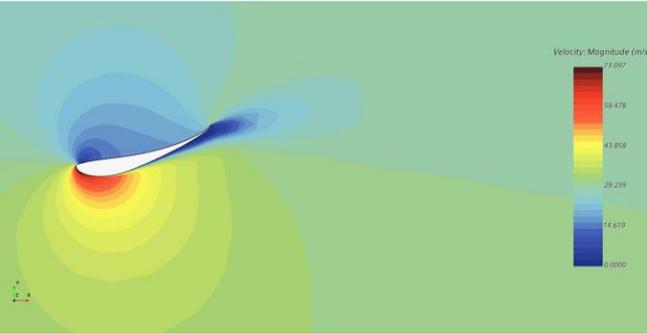
NACA 0012 C525 + C175



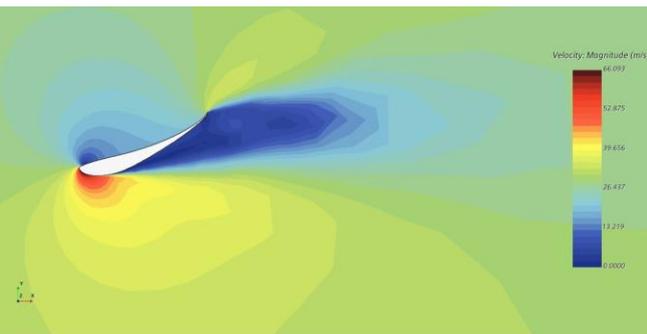
STALLO



PROFILO CURVO S 1223

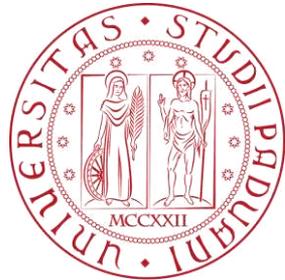
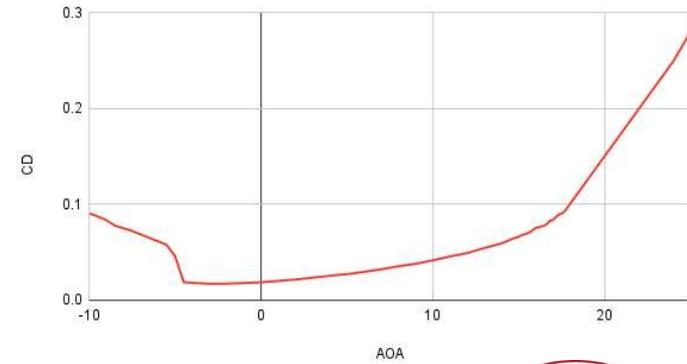
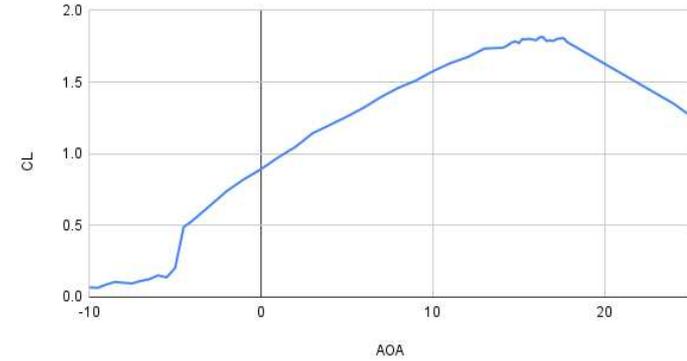


AOA 17° = STALLO INCIPIENTE



AOA 24° = STALLO PROFONDO

S1223 C650





$$\rho = 1.1352 \frac{kg}{m^3}$$

$$p = 99174.17 Pa$$

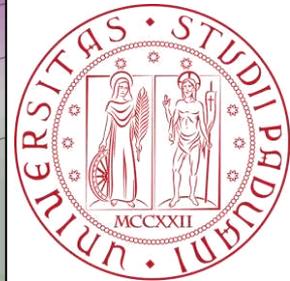
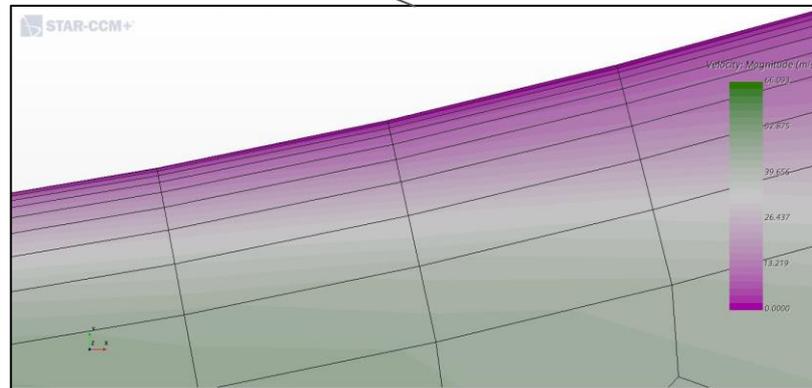
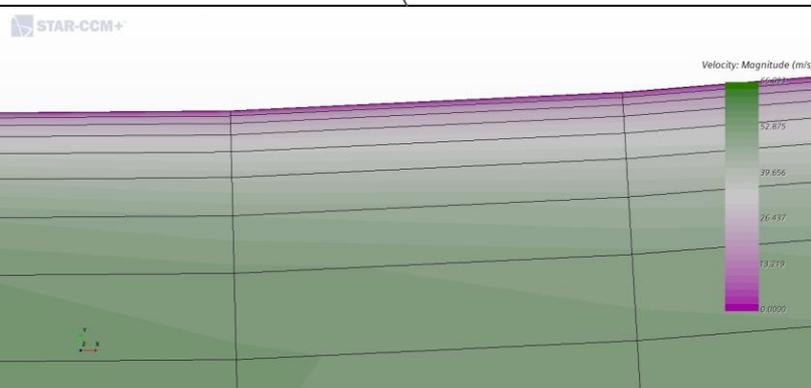
$$\mu = 1.868 * 10^{-5} Pa * s$$

$$Re = \frac{\rho V_{\infty} L_{\infty}}{\mu} \longrightarrow$$

Valori compresi
tra 6E4 e 2E6

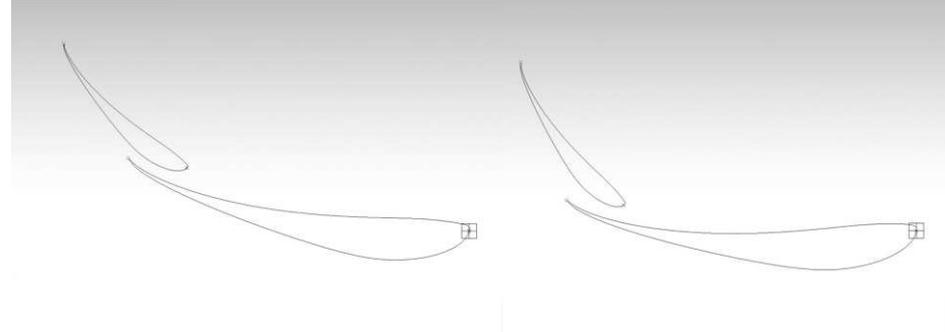
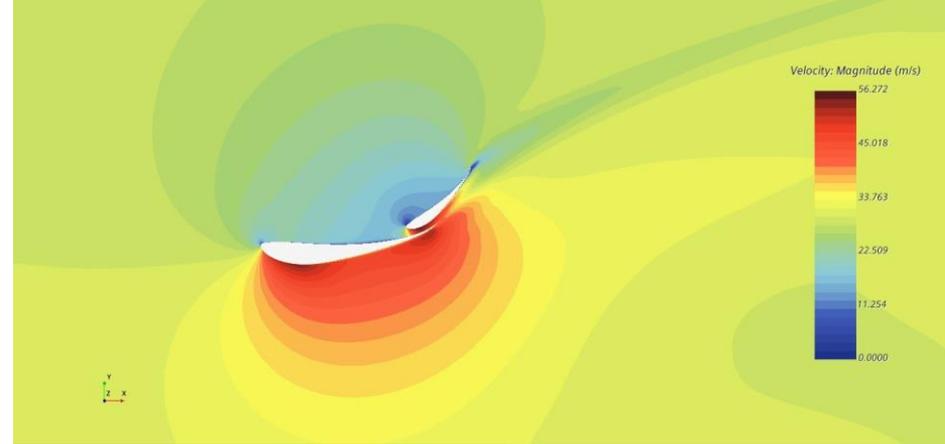
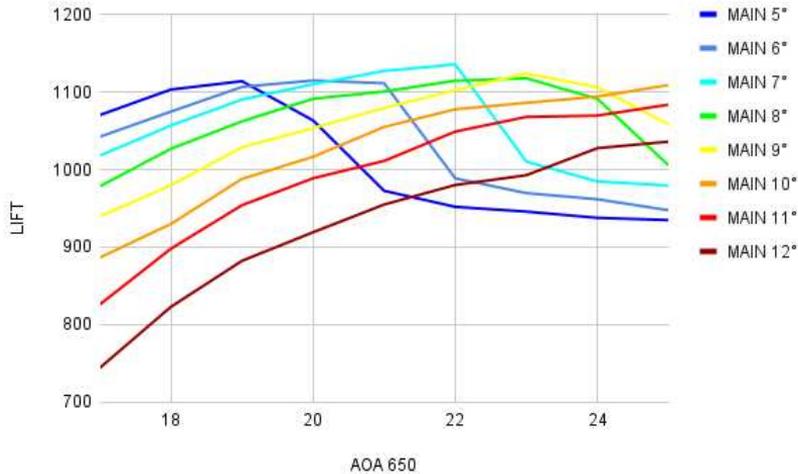
L'ANDAMENTO DELLA VELOCITA' NELLO STRATO LIMITE E' REGOLATO DALLA SEGUENTE RELAZIONE:

$$\frac{\delta^2 u}{\delta y^2} = \frac{dP_e}{dx}$$



PROFILO CURVO CON FLAP

Utilizzando 2 elementi, il cui insieme vada a formare un unico elemento di corda superiore, si raggiungono angoli d'attacco molto più elevati rispetto all'utilizzo di un singolo profilo, generando così maggior deportanza complessiva.



PASSAGGIO AL 3D

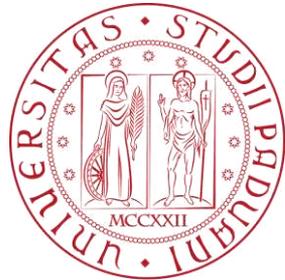
Conseguentemente ai vortici di estremità che deviano il flusso indisturbato, si verifica un aumento del drag ed una diminuzione della deportanza.

$$c_{D_i} = \frac{c_L^2}{\pi A Re}$$

$$c_L = 2\pi(\alpha - \alpha_i - \alpha_{L=0})$$



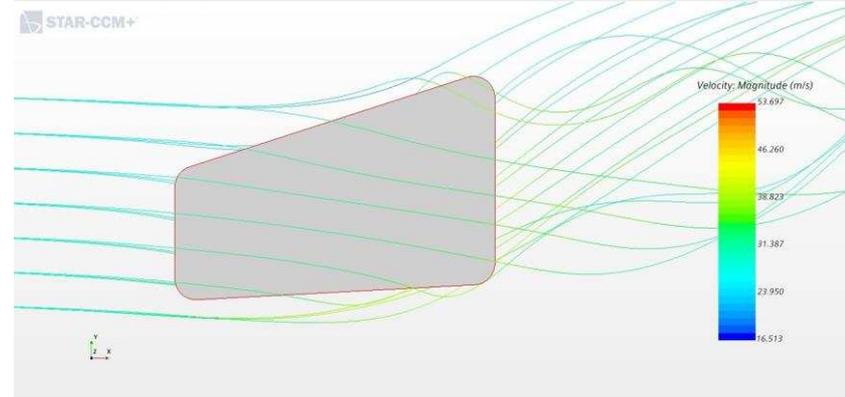
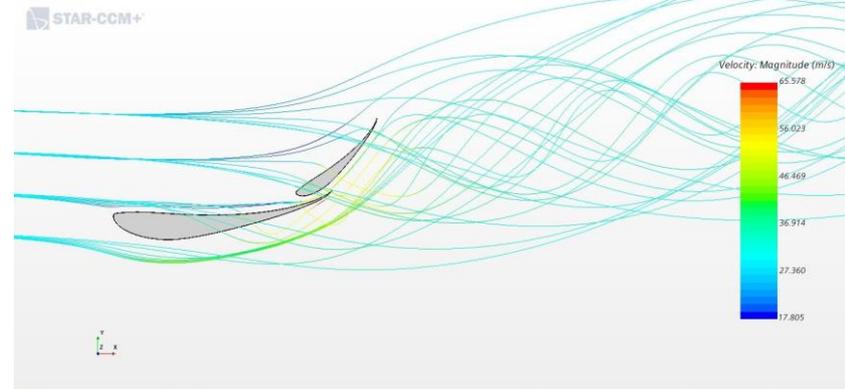
	2D	3D	DELTA
LIFT	1127.024	512.525	-54.524%
DRAG	44.266	200.158	+351.81%



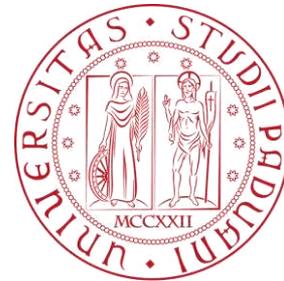
USO DI UN ENDPLATE

Una soluzione semplice quanto efficace è quella di impedire al flusso di andare a colmare il gap di pressione che si crea tra estradosso ed intradosso.

Così come negli aerei di linea, anche qui l'utilizzo dell'endplate è fondamentale all'estradosso, ossia dove la pressione è minima.

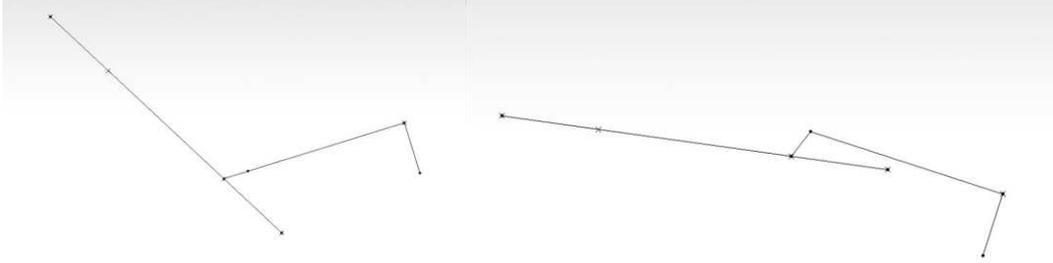
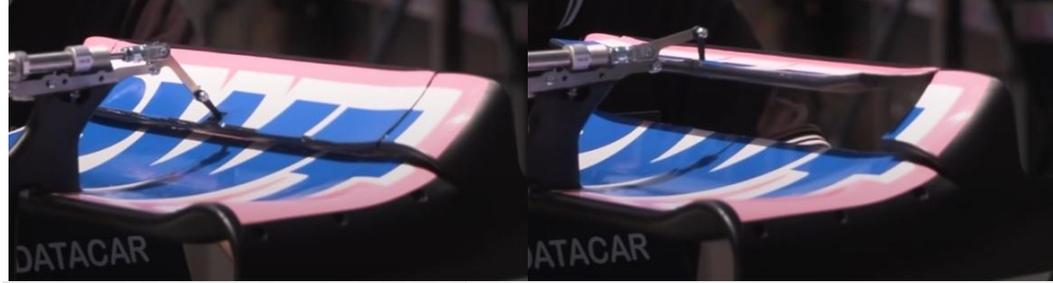


	NO ENDPLATE	ENDPLATE	DELTA
LIFT	512.525	645.616	+20.615%
DRAG	200.158	201.876	+0.86%

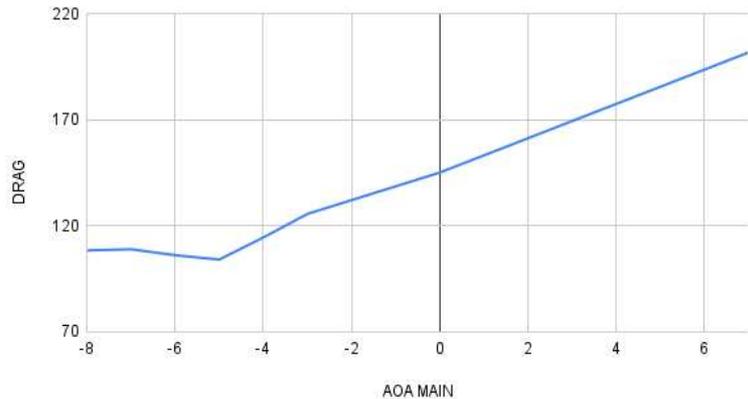


IL DRS

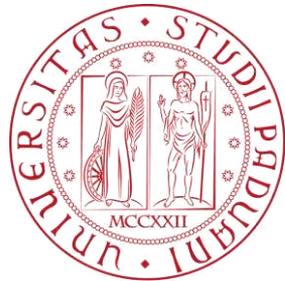
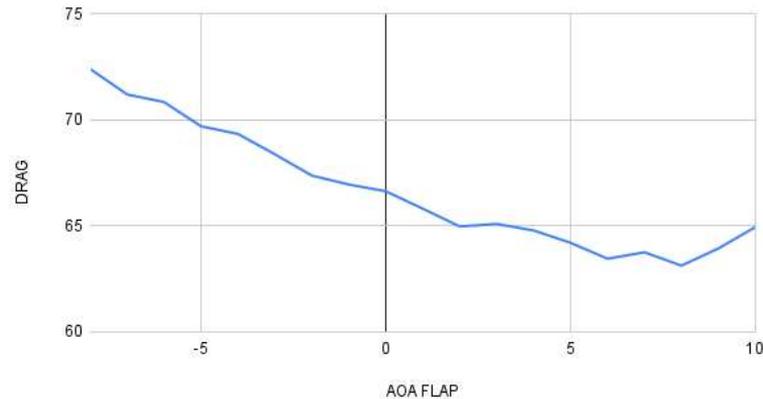
Supponiamo di voler ridurre la resistenza all'avanzamento con il vincolo di poter ruotare un solo profilo.

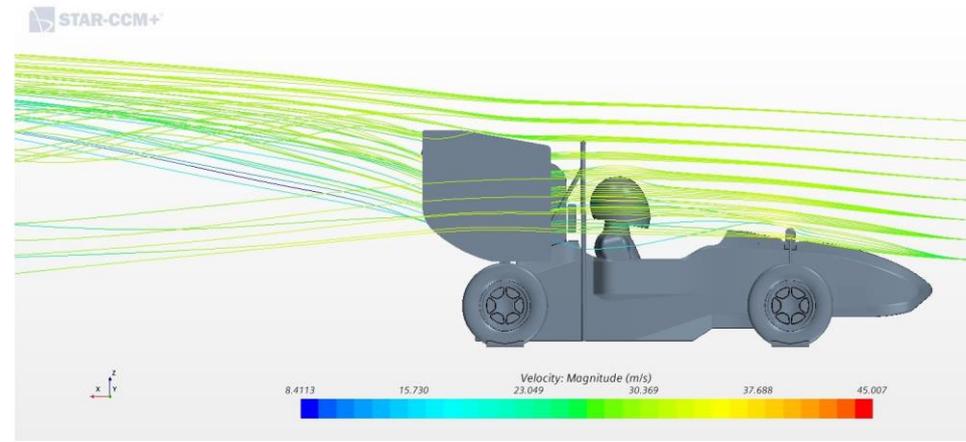
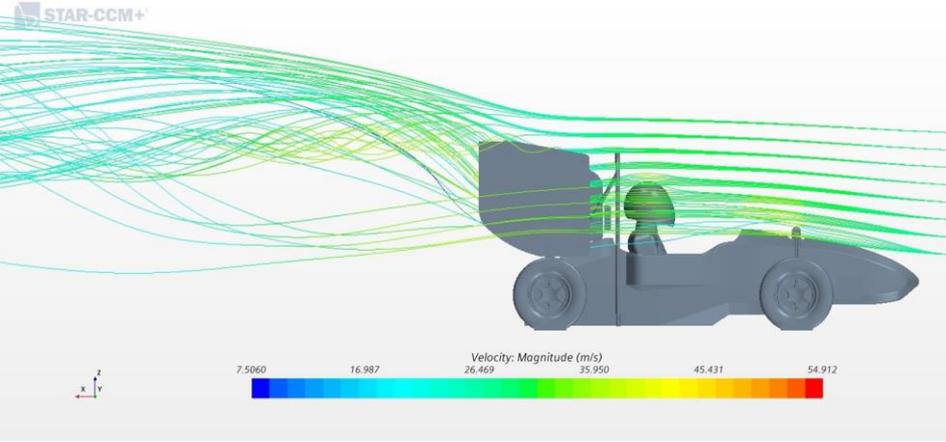


DRS MAIN PROFILE

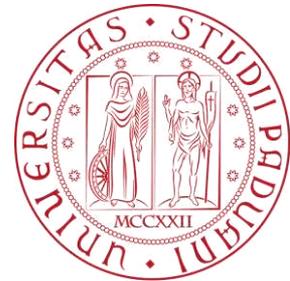


DRS FLAP





		LIFT TOT	DRAG TOT	LIFT ALA	DRAG ALA
ALA LIBERA	NO DRS			645.616	201.876
	DRS			314.187	63.131
MACCHINA	NO DRS	429.636	503.485	559.346	169.751
	DRS	166.45	343.572	286.591	60.630



GRAZIE PER L'ATTENZIONE

